

# Real-Time Optimization and Nonlinear Model Predictive Control for a Post-Combustion Carbon Capture Absorber

21<sup>st</sup> IFAC World Congress: July 13<sup>th</sup>-17<sup>th</sup>, 2020

Gabriel D. Patrón

Luis A. Ricardez-Sandoval

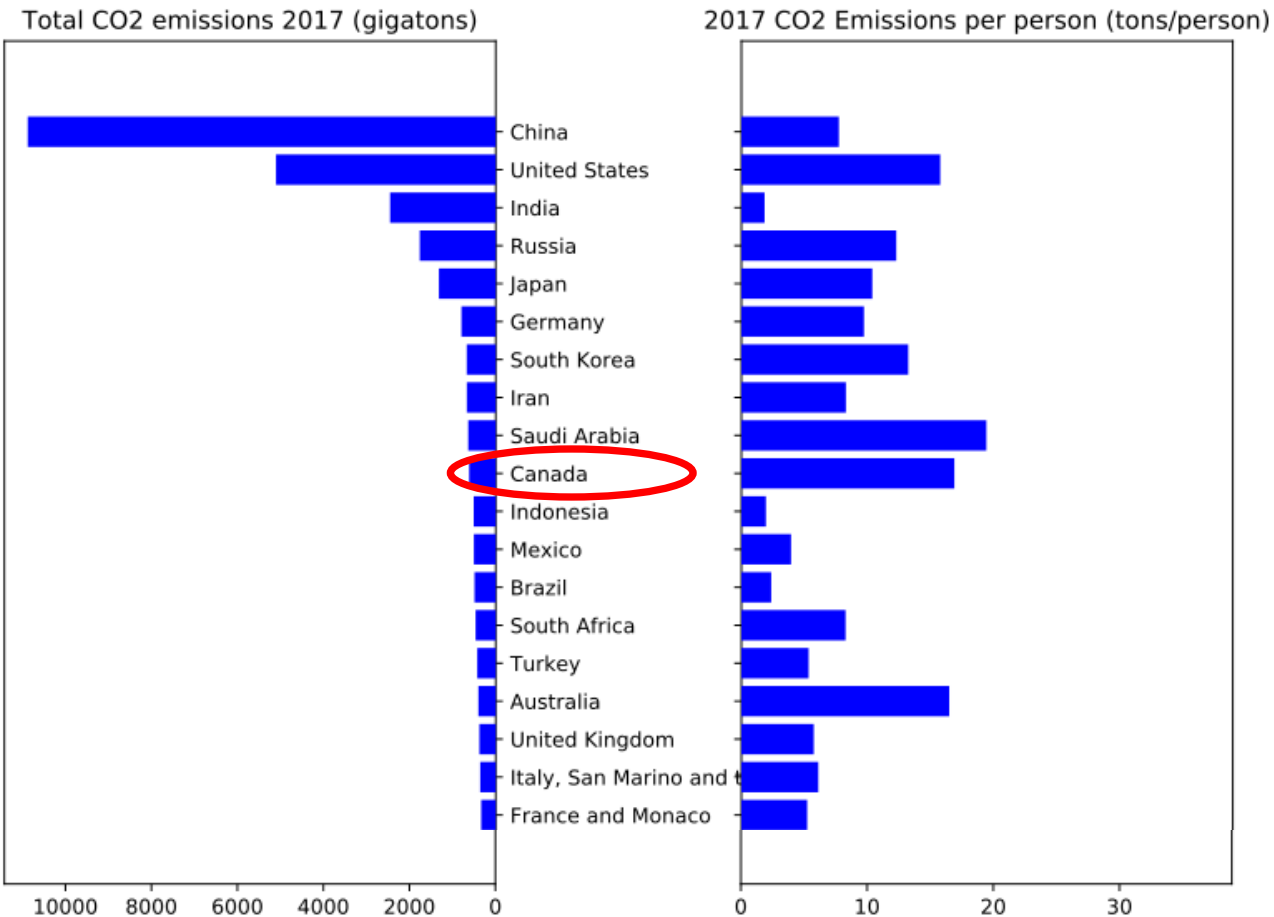
Department of Chemical Engineering



# Table of Contents

1. Motivation, challenges, and objectives
2. Model, implementation, and formulation
3. Test conditions and results
4. Conclusions and Future Work

# The CO<sub>2</sub> problem



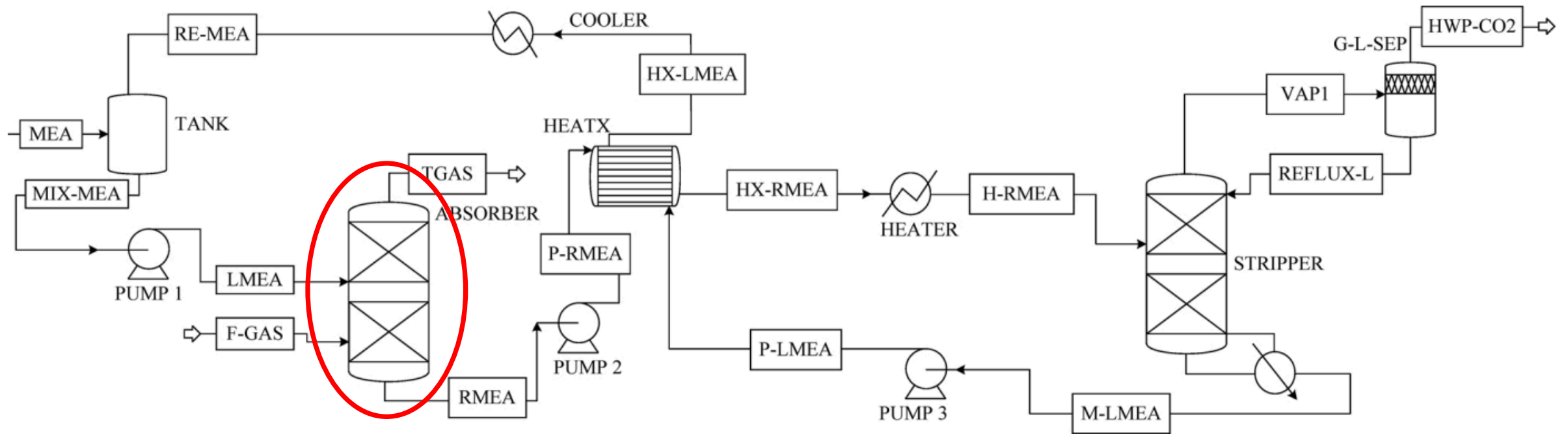
Muntean, M., Guizzardi, D., Schaaf, E., Crippa, M., Solazzo, E., Olivier, J. and Vignati, E. (2018). *Fossil CO2 Emissions of All World Countries: 2018 Report*. Luxembourg: Joint Research Centre (European Commission).

## CO2 capture methods

- Pre-combustion
- Oxy-combustion
- Chemical looping combustion
- Post-combustion (PCC)\*

\*most mature technology

# MEA Solvent Post Combustion Carbon Capture (PCC) System



L. Teck Chan and J. Chen. Economic model predictive control of an absorber-stripper CO<sub>2</sub> capture process for improving energy cost. IFAC-PapersOnLine, vol. 51, no. 18, pp. 109-114, 2018.

# PCC economic operation and control

- Nonlinear model prediction control (NMPC)
  - Reduced order absorber model (Akeson et al.,2012)
  - Robust mechanistic absorber model (Patrón and Ricardez-Sandoval, 2020)
- Economical operation
  - Linear multivariable MPC for PCC plant (Panahi and Skogestad, 2012)
- Economic MPC
  - Chan and Chen (2018)
  - Decardi-Nelson, Liu and Liu (2018)

**A two-layer RTO approach has not been tested for the PCC**

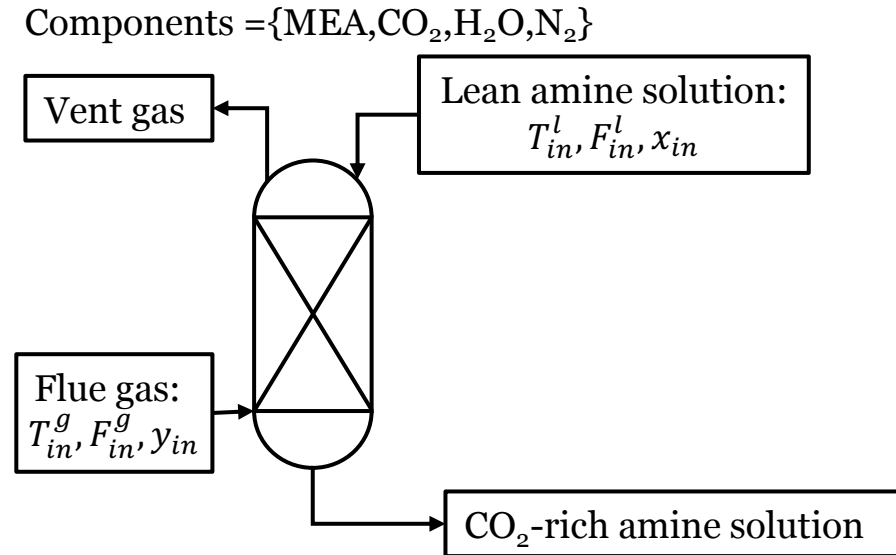
# Motivation, Challenges, and Objectives

## Motivation

- The absorber is of economic detriment to the upstream power plant
- The power plant introduces disturbances to the absorber, creating economic suboptimality

## Objectives

- Operate the absorber in an economically optimal way subject to upstream disturbances and changing carbon tax prices

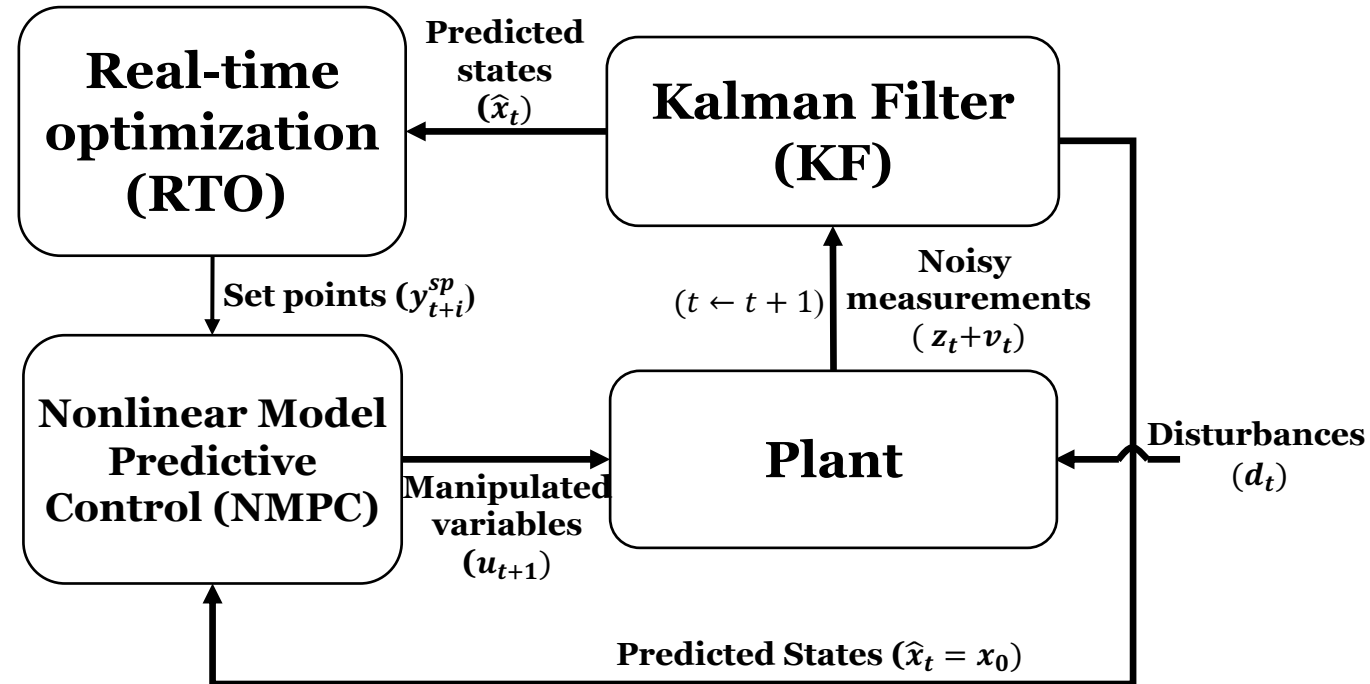


## Challenges

- Cost reduction and carbon capture are conflicting objectives
- State estimation is required

# Research objectives

- Novel RTO formulation for absorber
- Mechanistic process model in RTO and NMPC layer
- State estimation for absorber



\*all methods require models

# Differential Model of CO<sub>2</sub> Absorber Column - $f(x)$ \*

$i = \text{MEA}, \text{CO}_2, \text{H}_2\text{O}, \text{N}_2$

\* Adapted from Harun et al. (2012)

	Mass
Liquid	$\frac{dC_i^l}{dt} = u_l \frac{\partial C_i^l}{\partial z} + a_w N_i$
Gas	$\frac{dC_i^g}{dt} = -u_g \frac{\partial C_i^g}{\partial z} - a_w N_i - C_i^g \frac{\partial u_g}{\partial z}$
	Energy
Liquid	$\frac{dT_l}{dt} = u_l \frac{\partial T_l}{\partial z} - \frac{a_w}{\sum_{i=1}^4 c_{p,i}^l C_i^l} [h_{gl}(T_l - T_g) + \Delta H_{rxn} N_{\text{CO}_2} - \Delta H_{\text{H}_2\text{O}}^{\text{vap}} N_{\text{H}_2\text{O}} + h_{out}(T_l - T_{amb})]$
Gas	$\frac{dT_g}{dt} = -u_g \frac{\partial T_g}{\partial z} + \frac{a_w}{\sum_{i=1}^4 c_{p,i}^g C_i^g} [h_{gl}(T_l - T_g)]$

- Phenomenological and physical property equations ( $h(x)$ )
- Non-discretized model has 12 PDEs and 160 AEs



# Model Implementation

- PDAEs discretized by finite differences in axial domain and orthogonal collocations in time domain
- Model size (after discretization):
  - Axially (RTO)  $\Rightarrow$   $\sim 2,000$  nonlinear algebraic equations
  - Axially and temporally (NMPC)  $\Rightarrow$   $\sim 64,000$  nonlinear algebraic equations
- IPOPT (Wächter and Biegler, 2005)



# RTO Formulation

- Steady-state optimization
- Three sources of cost:
  - MEA degradation (per tonne of CO<sub>2</sub> removed)
  - Carbon Tax (per tonne of CO<sub>2</sub> emitted)
  - Electricity

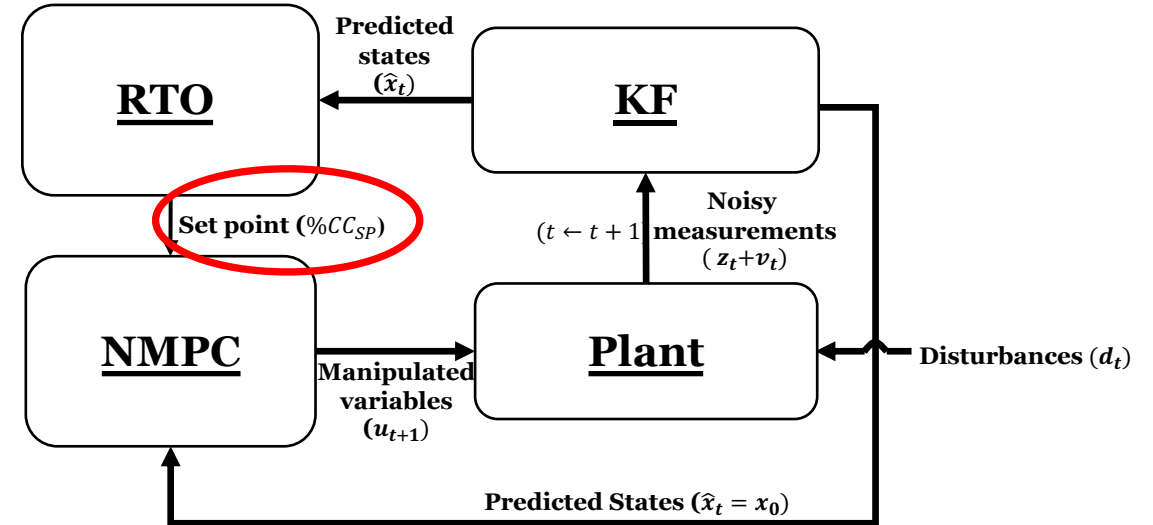
$$\min_{\%CC_{SP}} P_{MEA} \dot{m}_{CO_2, out}^l + P_{CO_2} \dot{m}_{CO_2, out}^g + P_e W_{pump}$$

s. t.

$$f(x_t, u_t) = 0$$

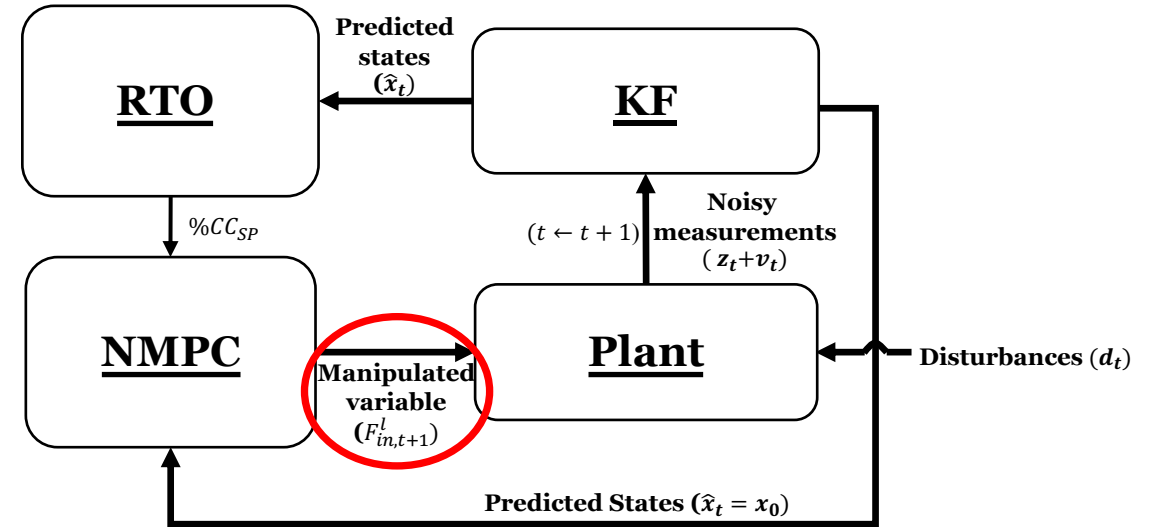
$$h(x_t, u_t) = \hat{Y}_t$$

$$u^l \leq u_t \leq u^h$$



# NMPC Formulation

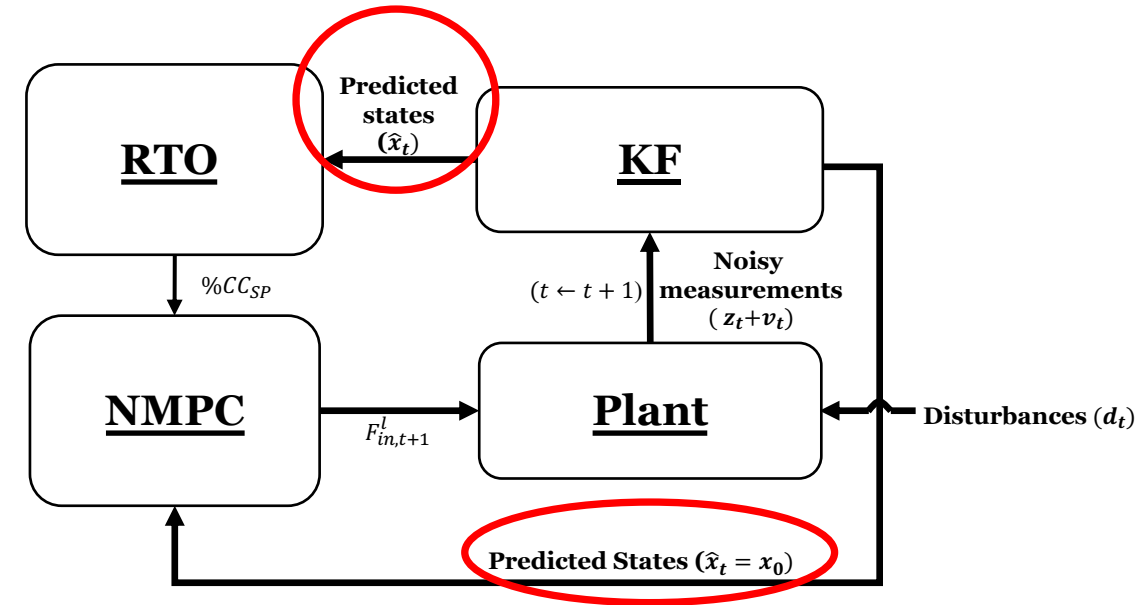
- Dynamic optimization
- Tracking and move suppression terms
- Manipulated variable bounds



$$\begin{aligned}
 & \min_{F_{in,t+j}^g \forall j \in \{1, \dots, C\}} Q \sum_{i=1}^P (\widehat{\%CC}_{t+i} - \%CC_{SP})^2 + R \sum_{j=1}^C \Delta F_{in,t+j}^l{}^2 \\
 & s. t. \\
 & f(x_t, u_{t+j}) = \hat{x}_{t+i}; \quad \forall i \in \{1, \dots, P\} \\
 & \quad \quad \quad \forall j \in \{1, \dots, C\} \\
 & x_t = x_0 \\
 & h(\hat{x}_{t+i}, u_{t+j}) = \hat{Y}_{t+i}; \quad \forall i \in \{1, \dots, P\} \\
 & \quad \quad \quad \forall j \in \{1, \dots, C\} \\
 & F_{in}^{l,l} \leq F_{in,t+j}^l \leq F_{in}^{l,u}; \quad \forall j \in \{1, \dots, C\}
 \end{aligned}$$

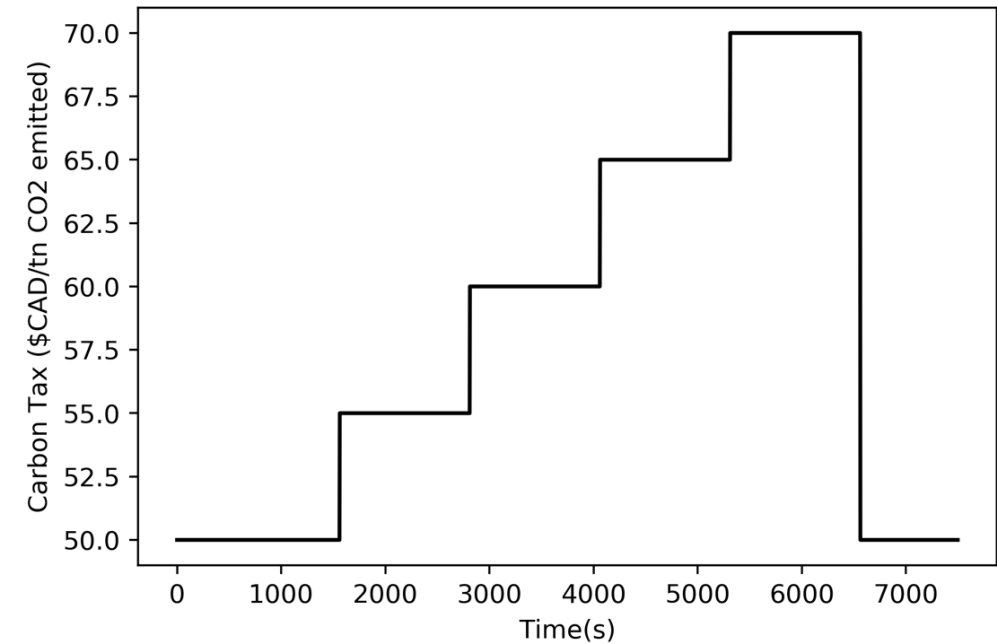
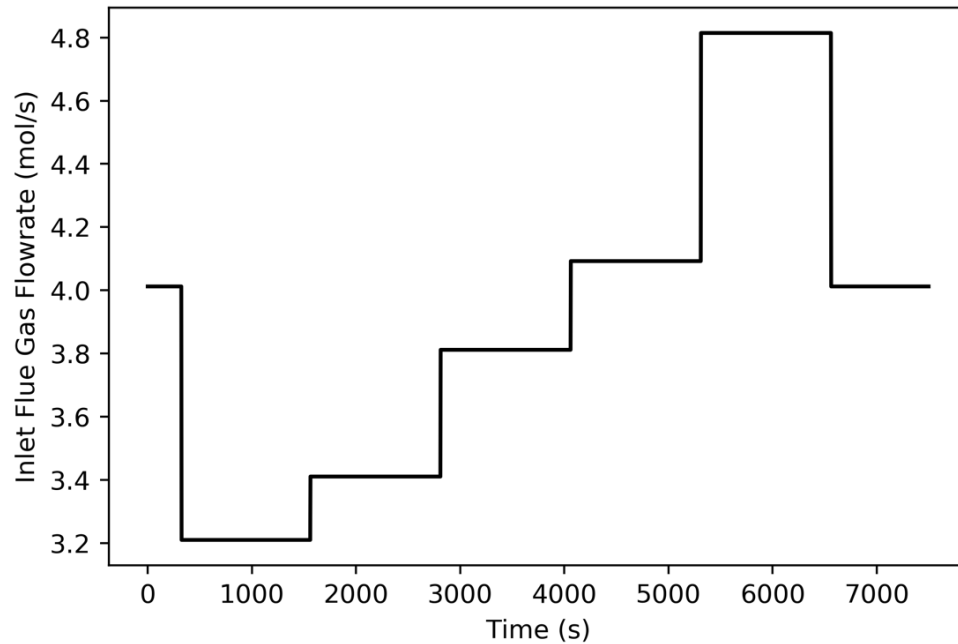
# KF Formulation

- 74/110 states measured
  - Temperatures, gas concentrations, inlet/outlet states
- *A priori* predictions generated using mechanistic model
- Jacobian matrix for generated symbolically
  - $\hat{x}_{k|k-1} = f(\hat{x}_{k-1|k-1}, u_k)$
  - $P_{k|k-1} = J_f P_{k-1|k-1} J_f^T + Q_k$
  - $K_k = P_{k|k-1} J_h^T (J_h P_{k|k-1} J_h^T + R_k)^{-1}$
  - $\hat{x}_{k|k} = \hat{x}_{k|k-1} + K_k (z_k - H_k \hat{x}_{k|k-1})$
  - $P_{k|k} = (I - K_k J_h) P_{k|k-1}$



# Results (test scenarios)

1. NMPC only (no RTO)
2. RTO (carbon tax at fixed 50 \$CAD/tn CO<sub>2</sub> emitted)
3. RTO (time-varying carbon tax)



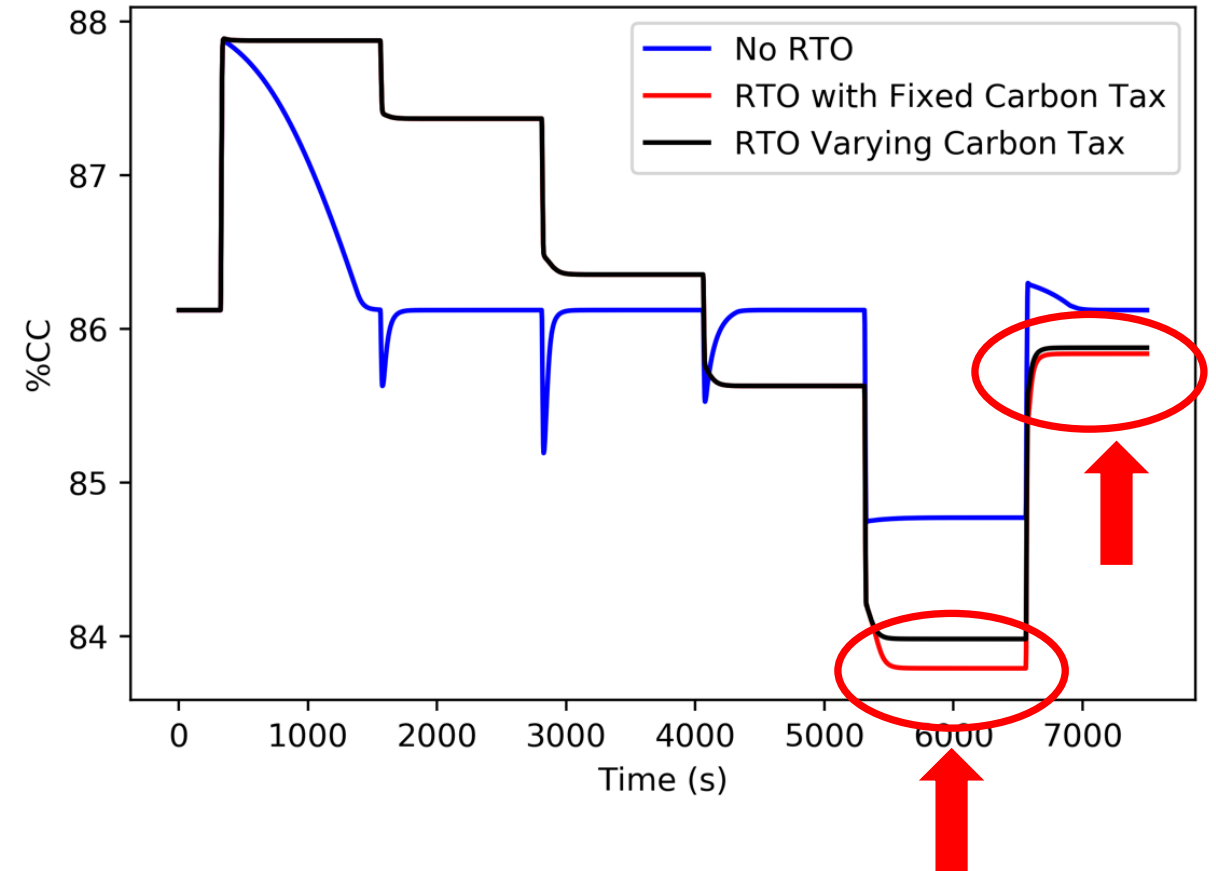
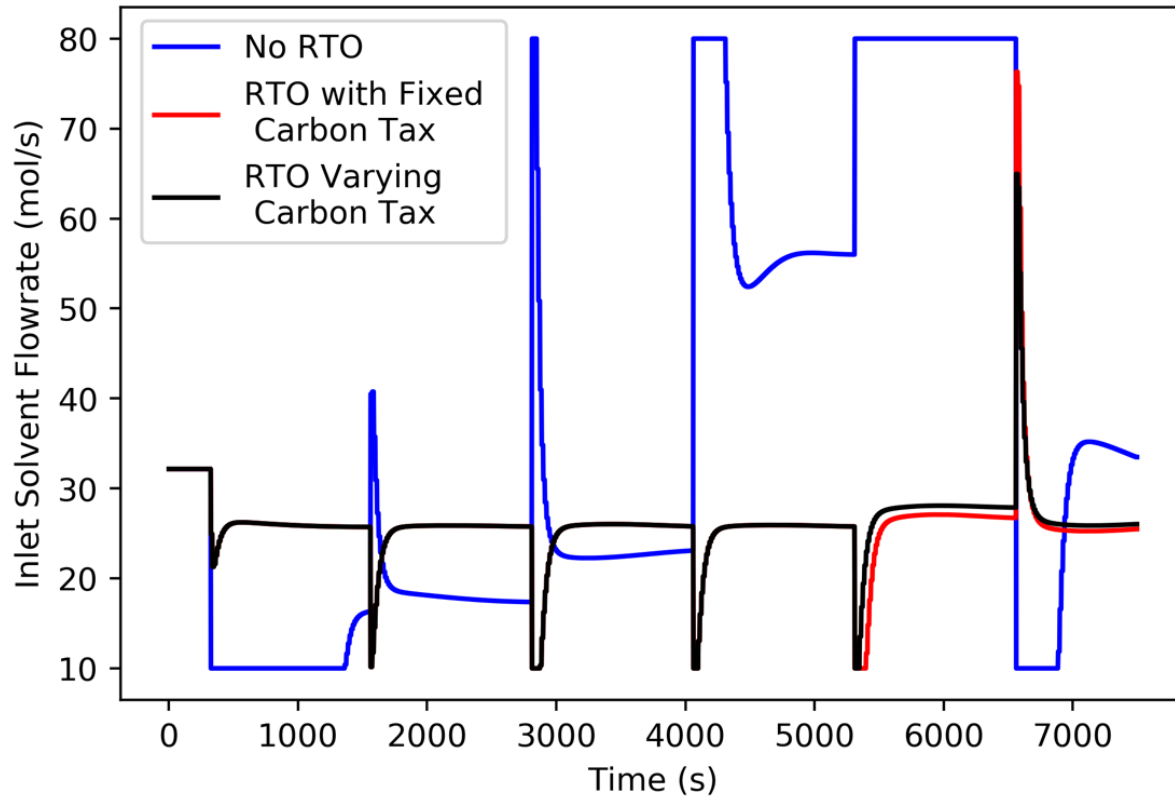
# Result (process cost)

\*costs in \$CAD

Scenario	Total Cost	Tax Cost	MEA Cost	Electrical Cost
No RTO (fixed tax)	13.46	6.31	7.13	0.01
No RTO (varying tax)	14.64	7.50	7.13	0.01
RTO (fixed tax)	11.98	6.31	5.67	0.01
RTO (varying tax)	13.23	7.51	5.70	0.01

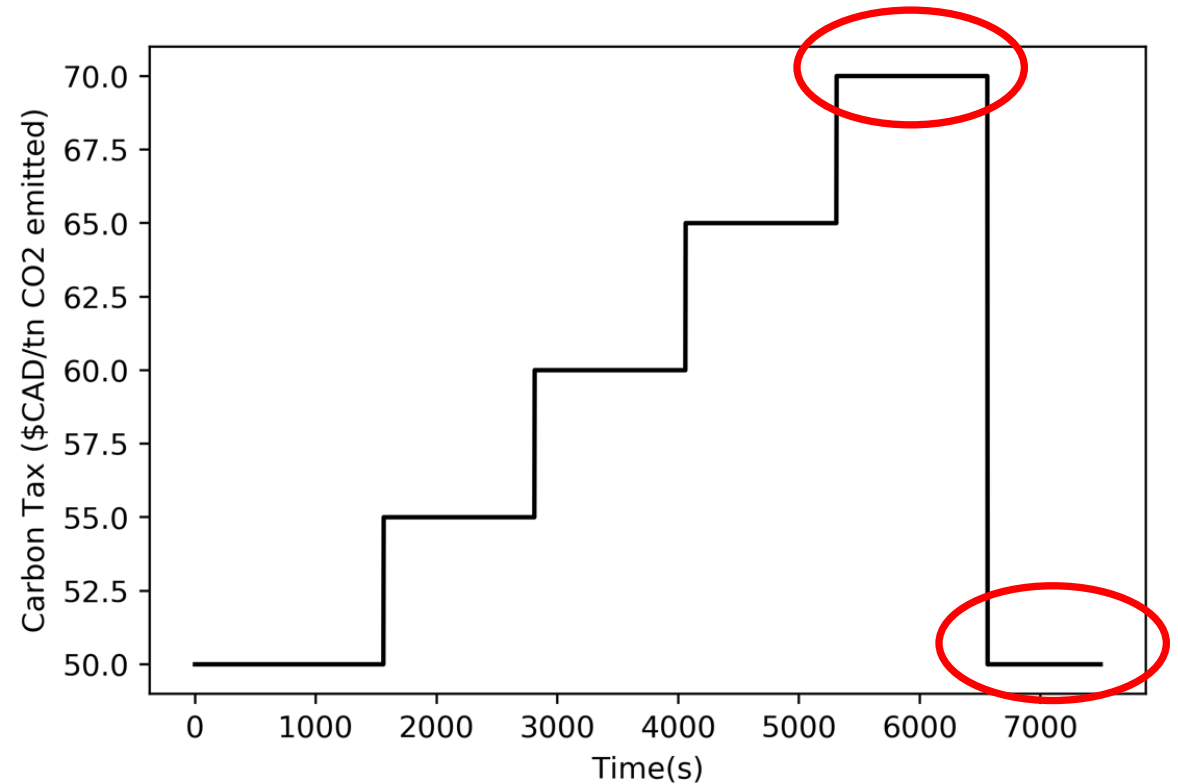
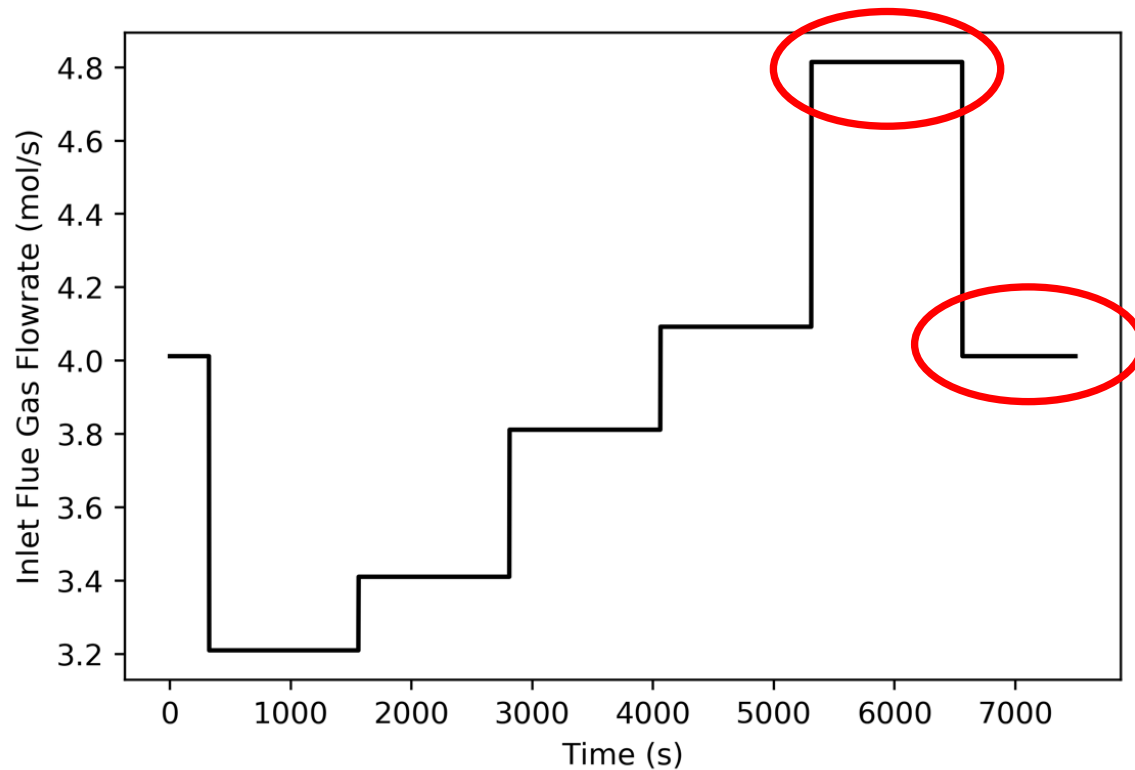
RTO sensitive to MEA cost

# Results (profiles)



- Fixed and varying tax case are only substantially different in final two RTO periods

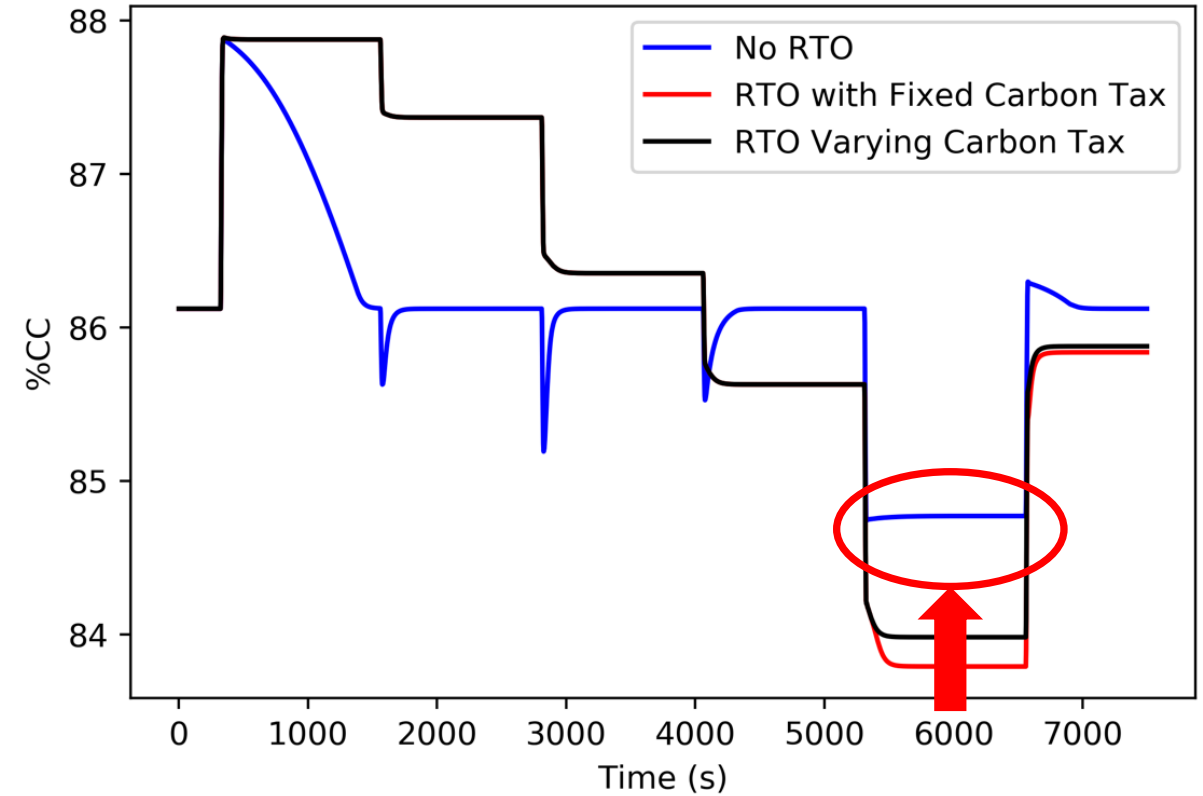
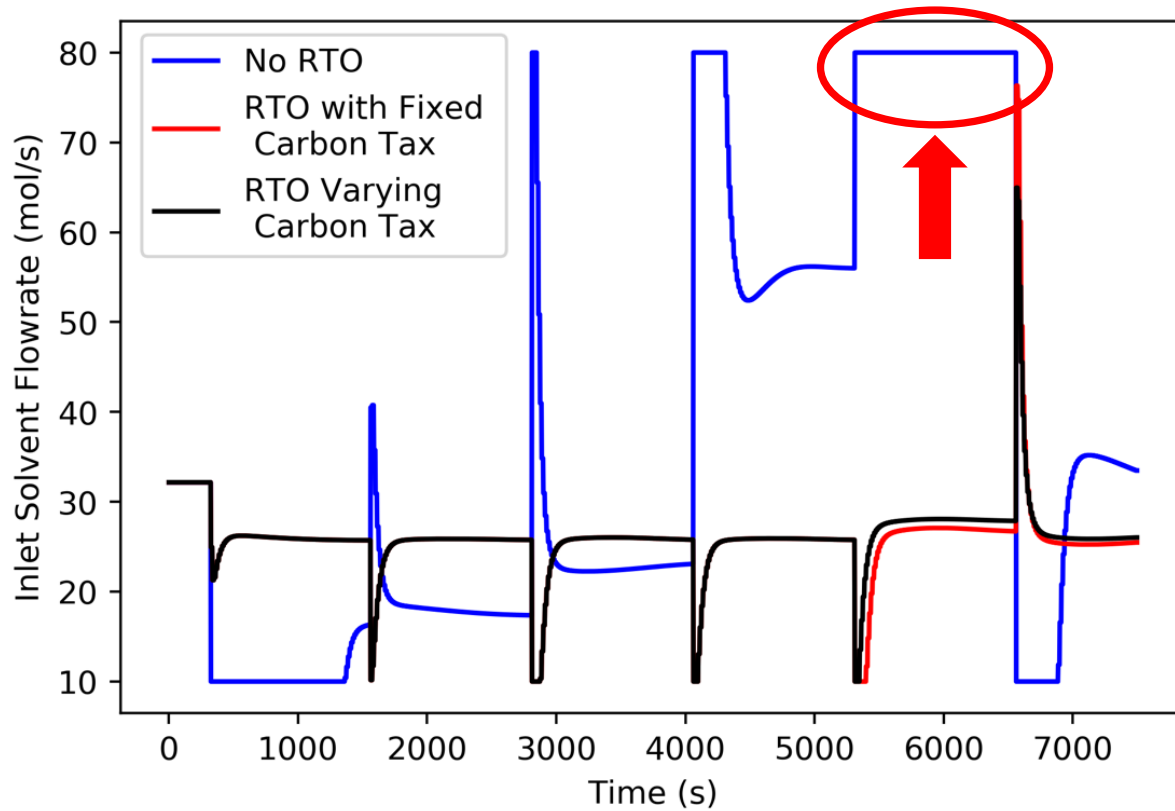
# Results (profiles)



- RTO only sensitive to tax rate when it coincides with large disturbances



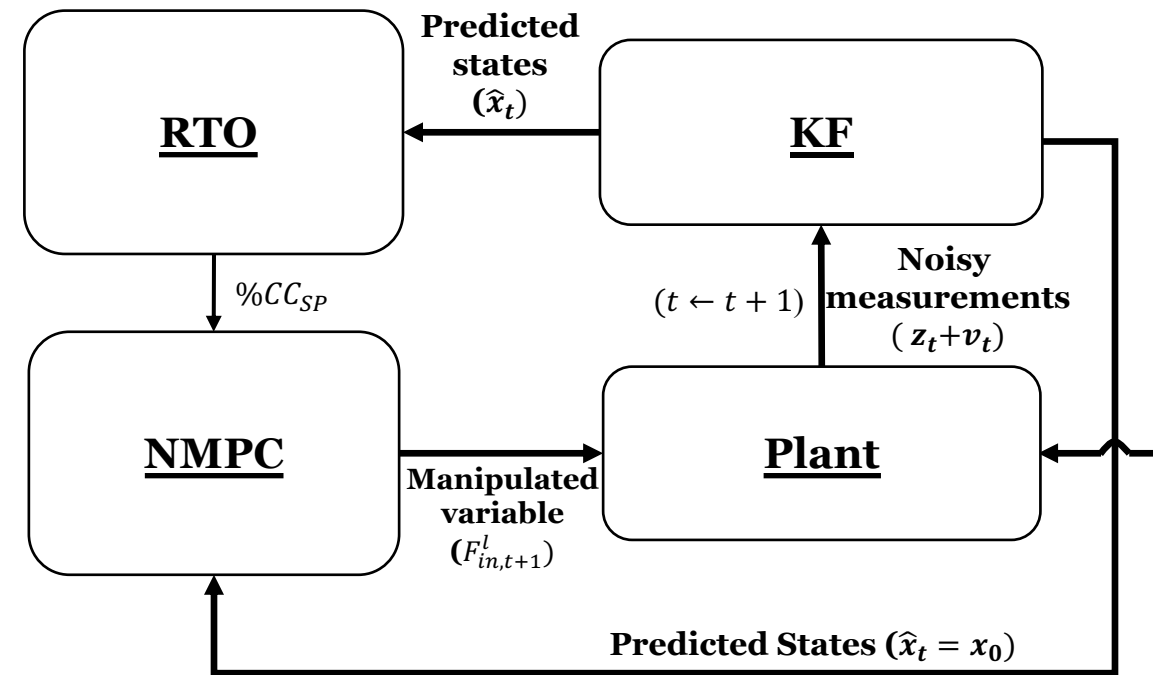
# Results (profiles)



- Large disturbances cause unreachable set points in no RTO scenario
- These are avoided by the executing the RTO

# Results (computational times)

	CPU time [s]	Number of equations	Key outputs
<b>RTO</b>	~15 s	1,861	1 ( $\%CC_{SP}$ )
<b>NMPC</b>	~60 s	64,480	9 ( $F_{in,t+1}^l$ )
<b>KF (a priori)</b>	~4 s	1,861	110 ( $\hat{x}_t$ )
<b>KF (a posteriori)</b>	<1 s	110	



# Conclusions

- RTO provides substantial economic benefit and avoids unreachable setpoints
- Carbon tax rate only impacts economics when under large disturbances
- KF is able to compute states at a computational cost

# Future Work

- Investigate more advanced estimation schemes (i.e. moving horizon estimation)
- Account for plant—model mismatch via parameter or modifier adaptation
- Merge RTO and NMPC layers by formulating an economic NMPC
- Consider entire post-combustion CO<sub>2</sub> plant (i.e. stripper, heat exchange units, tanks)



***NSERC  
CRSNG***

**Thank you**

[g2patron@uwaterloo.ca](mailto:g2patron@uwaterloo.ca)

[laricardezsandoval@uwaterloo.ca](mailto:laricardezsandoval@uwaterloo.ca)

<https://uwaterloo.ca/chemical-process-optimization-multiscale-modelling-process-systems/>

# References

- Åkesson, J., Laird, C., Lavedan, G., Prölb, K., Tummescheit, H., Velut, S. and Zhu, Y. (2012). Nonlinear Model Predictive Control of a CO<sub>2</sub> Post-Combustion Absorption Unit. *Chemical Engineering & Technology*, 35(3), pp.445-454.
- Auc.ab.ca. (2019). *Current rates and terms of conditions*. [online] Available at: <http://www.auc.ab.ca/Pages/current-rates-electric.aspx> [Accessed 10 Oct. 2019].
- Canada.ca. (2019). *Pricing carbon pollution in Canada: how it will work*. [online] Available at: [https://www.canada.ca/en/environment-climate-change/news/2017/05/pricing\\_carbon\\_pollutionincanadahowitwillwork.html](https://www.canada.ca/en/environment-climate-change/news/2017/05/pricing_carbon_pollutionincanadahowitwillwork.html) [Accessed 10 Oct. 2019].
- Chan, L. and Chen, J. (2018). Improving the energy cost of an absorber-stripper CO<sub>2</sub> capture process through economic model predictive control. *International Journal of Greenhouse Gas Control*, 76, pp.158-166.
- Decardi-Nelson, B., Liu, S. and Liu, J. (2018). Improving Flexibility and Energy Efficiency of Post-Combustion CO<sub>2</sub> Capture Plants Using Economic Model Predictive Control. *Processes*, 6, 135.
- Hart W, Watson J, Woodruff D. (2011). Pyomo: modeling and solving mathematical programs in Python. *Mathematical Programming Computation*, 3(3):219–60.
- Harun, N., Nittaya, T., Douglas, P., Croiset, E. and Ricardez- Sandoval, L. (2012). Dynamic simulation of MEA absorption process for CO<sub>2</sub> capture from power plants. *International Journal of Greenhouse Gas Control*, 10, pp.295-309.
- Panahi, M. and Skogestad, S. (2012). Economically efficient operation of CO<sub>2</sub> capturing process. Part II. Design of control layer. *Chemical Engineering and Processing: Process Intensification*, 52, pp.112-124.
- Patron, G. and Ricardez-Sandoval, L., 2020. A robust nonlinear model predictive controller for a post- combustion CO<sub>2</sub> capture absorber unit. *Fuel*, 265, 116932.
- Wächter A, Biegler L. (2005). On the implementation of an interior-point filter line-search algorithm for large-scale nonlinear programming. *Mathematical Programming*, 106(1):25–57.